

ECE 388 – Automatic Control

Steady-State and Transient Response of LTI Systems

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Compulsory Course in Electronic and Communication
Engineering
Credits (2/2/3)

Course Webpage: <http://ECE388.cankaya.edu.tr>

Responses: Separation

Transient Response

Response of a system to an input signal for a short time period after the application of the input signal: $y_{tr}(t)$

Steady-State Response

Long term response of a system to an input signal after the transient response vanishes: $y_{ss}(t)$

Separation

$$y(t) = y_{tr}(t) + y_{ss}(t)$$

Remark

If stability of a control system is ensured, it is desired to shape the transient response of the control system

Responses: Example

Computation

Gap 1

Responses: Properties

Properties

- If $G(s)$ is BIBO stable, then the transient response converges to zero

$$\lim_{t \rightarrow \infty} y_{tr}(t) = 0$$

- If $G(s)$ is unstable, then the transient response diverges

$$\lim_{t \rightarrow \infty} |y_{tr}(t)| = \infty$$

- Steady state response for LTI systems is determined by the input

Example

Gap 2

Responses: Example

Computation

Gap 3

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Properties of the Steady-State Response: Final Value

Final Value Theorem

- If $\lim_{t \rightarrow \infty} y(t)$ exists:

$$\lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} s Y(s)$$

- Final value for the step response of a stable transfer function $G(s)$

$$\lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} s G(s) \frac{1}{s} = \lim_{s \rightarrow 0} G(s)$$

Example

Gap 4

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Properties of the Transient Response: Distinct Poles

Step Response

$$Y(s) = G(s) \frac{1}{s} = K \frac{(s - z_1)(s - z_2) \cdots (s - z_m)}{(s - p_1)(s - p_2) \cdots (s - p_n)} \frac{1}{s}$$

Decomposition for Distinct Poles

Gap 5

$$\Rightarrow Y(s) = \frac{r_0}{s} + \frac{r_1}{s - p_1} + \frac{r_2}{s - p_2} + \cdots + \frac{r_n}{s - p_n}$$

→ p_1, p_2, \dots, p_n are called the modes of the system

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Properties of the Transient Response: Example

Computation

Gap 6

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Properties of the Transient Response: Cases

Real Pole $p_i \neq 0$

$$\frac{r_i}{s - p_i} \bullet \longrightarrow \circ r_i e^{p_i t} \sigma(t)$$

$$\Rightarrow \lim_{t \rightarrow \infty} r_i e^{p_i t} \sigma(t) = \begin{cases} 0 & \text{if } p_i < 0 \\ \infty & \text{if } p_i > 0 \end{cases}$$

Comparison $p_i < p_j < 0$ and $r_i \approx r_j$

$$r_i e^{p_i t} \sigma(t) < r_j e^{p_j t} \sigma(t)$$

$\Rightarrow p_j$ dominates p_i

Comparison p_i, p_j but $r_j \ll r_i$

$$r_j e^{p_j t} \sigma(t) < r_i e^{p_i t} \sigma(t)$$

$\Rightarrow p_i$ dominates p_j

Illustration

Gap 7

Properties of the Transient Response: Example

Output Response

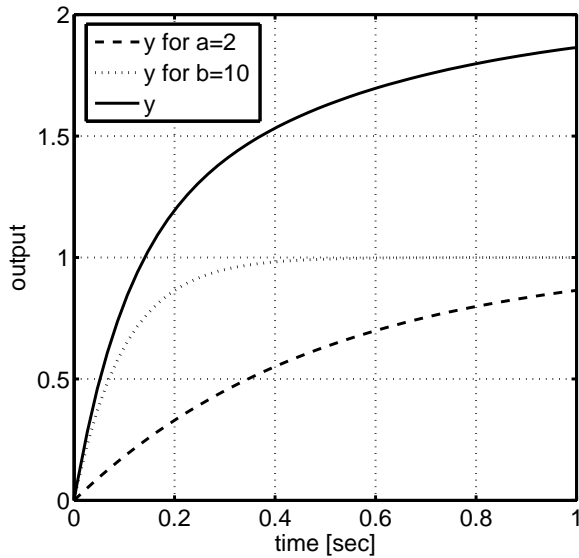
$$Y(s) = \frac{A/a + B/b}{s} - \frac{A/a}{s+a} - \frac{B/b}{s+b}$$

Computation

Gap 8

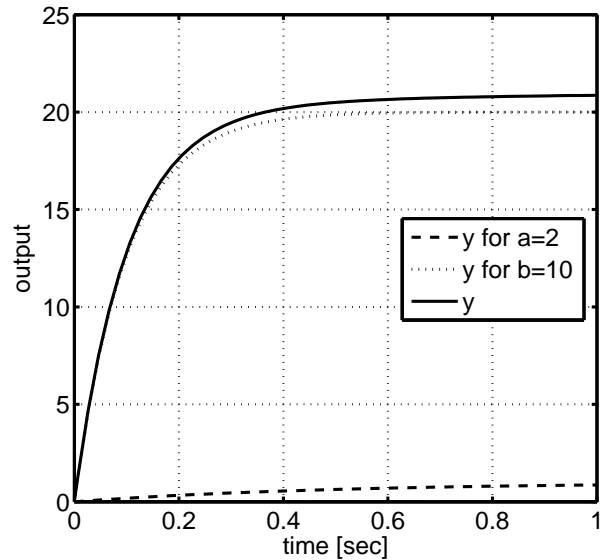
Properties of the Transient Response: Example

$$A/a = B/b$$



⇒ pole at a dominates pole at b

$$A/a \ll B/b$$



⇒ pole at b dominates pole at a

Properties of the Transient Response: Cases

Conjugated Complex Poles

$$\frac{r_i}{s - p_i} + \frac{r_i^*}{s - p_i^*} \bullet \circ 2 |r_i| e^{\operatorname{Re}(p_i) t} \cos(\operatorname{Im}(p_i) t + \angle(r_i))$$

Properties

$$\lim_{t \rightarrow \infty} 2 |r_i| e^{\operatorname{Re}(p_i) t} \cos(\operatorname{Im}(p_i) t + \angle(r_i)) = \begin{cases} 0 & \text{if } \operatorname{Re}(p_i) < 0 \\ \infty & \text{if } \operatorname{Re}(p_i) > 0 \end{cases}$$

⇒ exponential decay/increase similar to real pole

$$D = \frac{-\operatorname{Re}(p_i)}{|p_i|}$$

Gap 9

Dominant Poles: Relation

Conditions for Poles

- If there is an instable pole, it dominates all stable poles
- Usually, stable poles close to the imaginary axis (slow convergence) dominate stable poles far from the imaginary axis (fast convergence)
- Exceptions exist depending on the residues of the modes

Examples

Gap 10

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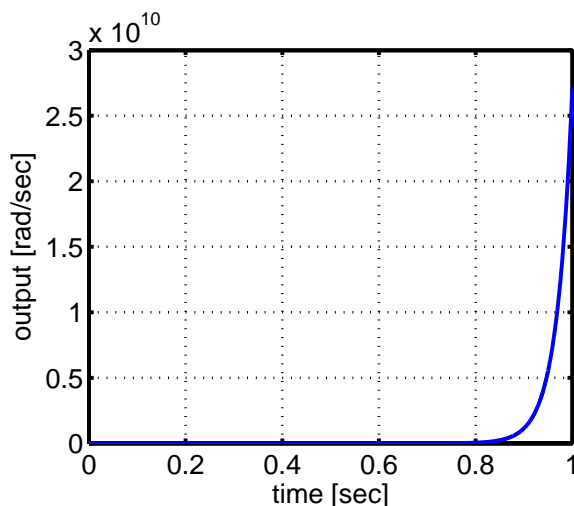
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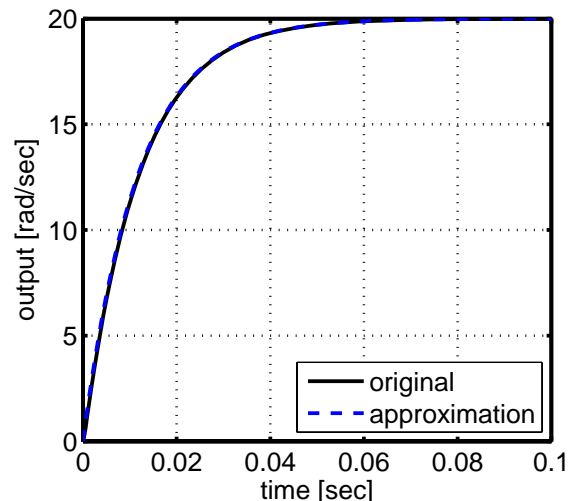
Dominant Poles: Simulation

Gap 11

Magnetic Suspension



DC Motor



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Plant Zeros: Basics

Stable Plant

$$G(s) = K \frac{(s - z_1) \cdots (s - z_m)}{(s - p_1) \cdots (s - p_n)}$$

Minimum-Phase Zero

- Zeros in the open left half plane: $\text{Re}(z_j) < 0$

Non-minimum Phase Zero

- Zero in the right half plane: $\text{Re}(z_j) > 0$

Example

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Plant Zeros: Minimum Phase Zeros and Dominant Poles

Suppression of Dominant Poles

- Assume a zero z_j is close to the dominant pole p_i : $z_j \approx p_i$

$$G(s) = \frac{(s - z_j)\tilde{B}(s)}{(s - p_i)\tilde{A}(s)}$$

- Residue of mode p for step response

$$r_i = \lim_{s \rightarrow p_i} \frac{G(s)(s - p_i)}{s} = \frac{(p_i - z_j)\tilde{B}(p_i)(s - p_i)}{(s - p_i)\tilde{A}(p_i)} \approx 0$$

- \Rightarrow Dominant mode with pole p_i does not appear in the step response
- \Rightarrow If $z_j \approx p_i$, dominant modes can be suppressed and other modes become dominant

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Plant Zeros: Minimum Phase Zeros and Dominant Poles

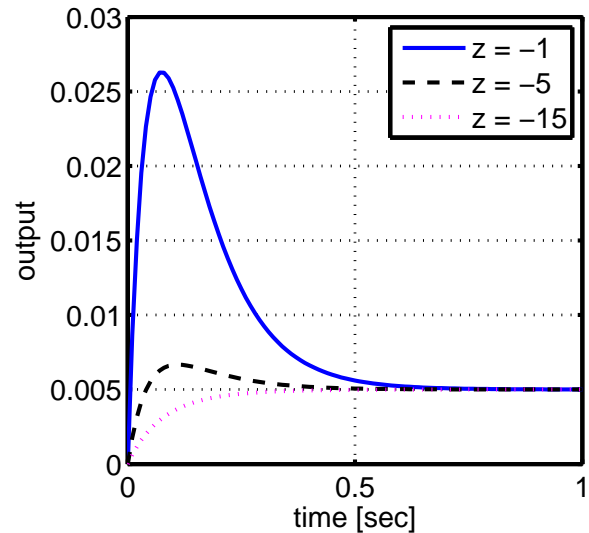
Overshoot

- Dominant plant pole at p with $\text{Re}(p) < 0$
- Slow minimum phase plant zero z with $\text{Re}(p) \ll \text{Re}(z) < 0$

⇒ Overshoot of the step response

Example Transfer Function

$$G(s) = \frac{-1}{z} \frac{(s - z)}{(s + 10)(s + 20)}$$



Plant Zeros: Non-minimum Phase

Statement

- k non-minimum phase zeros in $G(s)$
 - ⇒ Step response intersects with time-axis k times
 - ⇒ Undershoot whenever there are non-minimum phase zeros

Example

$$G(s) = \frac{5(s - 1)}{(s + 1)(1 + 30s)}$$

⇒ One intersection of the step response with the time axis

Example Simulation

